

MEASUREMENT OF WIDE- BANDGAP POWER DEVICES TIPS & GUIDELINES

Marcus Sonst
Senior Application Engineer Power Applications

ROHDE & SCHWARZ

Make ideas real



INTRODUCTION

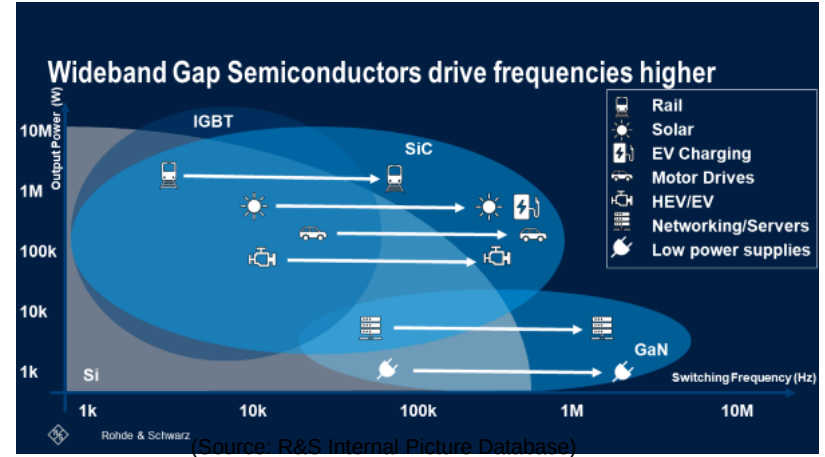
- ▶ Overview of WBG Technology
- ▶ Challenges In Measuring WBG Power Devices
- ▶ Essential Measurement Tools And Equipment, Probing Solutions And Their Impact
- ▶ Advanced Measurement Techniques For Device Characterization
- ▶ Case Study Of Switching Converter
- ▶ Conclusion / Q&A

WHY NEW MEASUREMENT METHODS?

- Wideband Gap Technology
 - Higher Switching Frequency
 - Less Parasitic Components

Benefits Are Efficiency And Compact Designs!!!

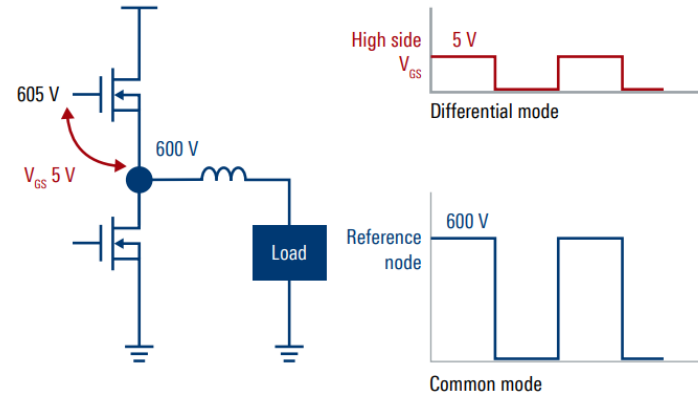
- Looking From A Measurement Perspective
 - Higher Bandwidth
 - Common Mode Noise (dv/dt)
 - Probing Itself Becomes Critical
 - Lower Gate Voltages
 - Filtering of EMI Emissions



COMMON MODE NOISE

- ▶ What is CM Noise?
 - Appears In Any Half-Bridge Structure
 - Caused By Turn-On And Turn-Off Of Power Switches At Switch Node
 - It Degrades Signal Fidelity
- ▶ Why Is It More Challenging Using WBG Devices?
 - Faster Rising And Falling Edges (dv/dt)
 - Measurement Tools Need To Suppress This Noise

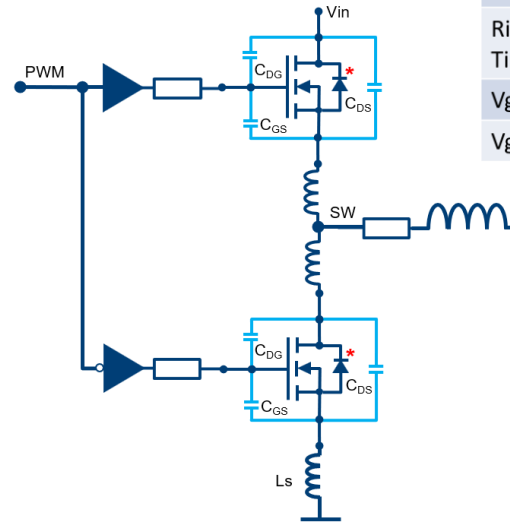
High-Side Gate Voltage & Current Shunt



(Source: R&S RT-ZISO Brochure)

PARASITIC COMPONENTS OF WBG

- ▶ WBG Devices Provide Lowest Parasitic Components C_{gs} , C_{oss} and C_{dg} Compare To Silicon Counterparts
- ▶ The Parasitic Elements Introduced By Probes Can Overlay The GaN Device Parameters And Lead To Erroneous Measurement Results
- ▶ More Critical Are The External Inductor Created By Loops in the PCB (di/dt)
>> Impact On Probing



Parameter	GaN 100V/6mΩ	Silicon 100V/6mΩ
$C_{iss} (C_{gd}+C_{gs})$	644pF	2025pF
C_{gd}	2,4pF	20pF
C_{ds}	304pF	468pF
Rise Time/ Fall Time	1,4ns	22ns/8ns
$V_{gs}(TH)$	1V	3V
$V_{gs} (on/off)$	5V/0V	10V/0V

(Source: Datasheet GaN2204/FDPF085N10A)

BANDWIDTH & RISE TIME & ACCURACY

- ▶ Estimation Of System Bandwidth (f_{BW}) Is Determined By Rise Time (t_r)
 - t_r : Transition time for a signal to go from the 10% to the 90% level of the steady maximum value
 - f_{BW} : Frequency range over which the frequency response of a signal degrades by 3 dB

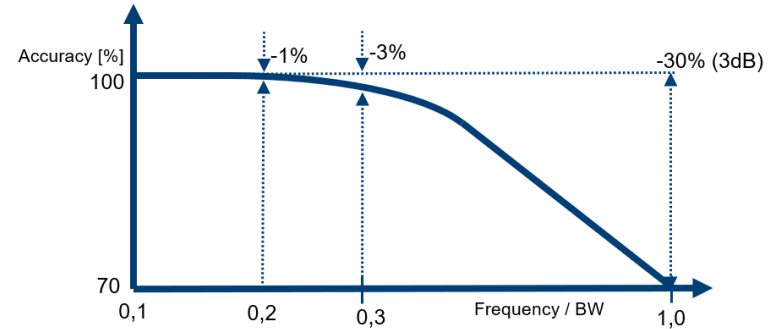
- ▶ Most Used Equation:

$$f_{BW} = 0.4 / t_r$$

- ▶ This Equation Would Be An Overestimation:

$$f_{max} = 1/t_r$$

- ▶ System Bandwidth Is Defined By Scope AND Probe

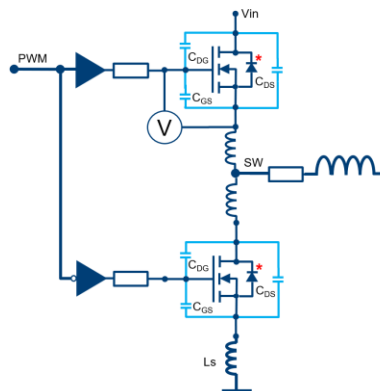


It is derived by considering a first-order passive filter and calculating its step-response in frequency and time domain.

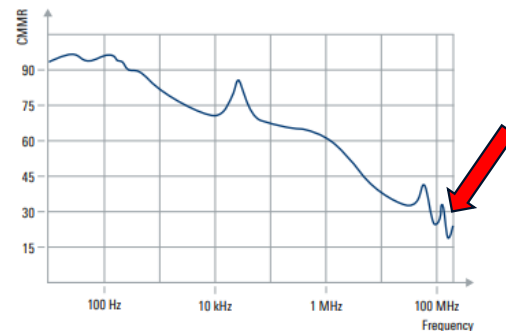
$$BW_{system} = \frac{1}{\sqrt{\left(\frac{1}{BW_{probe}}\right)^2 + \left(\frac{1}{BW_{scope}}\right)^2}}$$

CMRR FOR STANDARD DIFFERENTIAL PROBES

- ▶ Determining CMRR Requirement
 - High-Side Gate Measurement In the Presence Of High CM Noise
 $\gg dv/dt = 40V/2ns = 20V/ns$
 - Max. Failure < **2%** On HS-Gate
 - Voltage Failure[V] < **100mV** @ 5V
(On State of GaN Gate)
 - CMMR = $20 \cdot \log(0,1V/40V) = \mathbf{52dB}$
 - Suppression Is Required At >200MHz



CMRR for a typical high voltage differential probe in dB



(Source: R&S RT-ZISO Brochure)

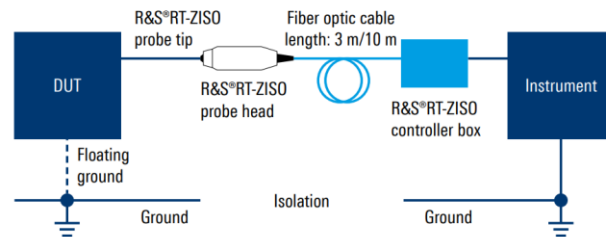
Traditional HV Differential Probes Will Fail Because Of Low CMMR
(30dB $\gg$ 25%) And Bandwidth Limitation

OPTICAL ISOLATED MEASUREMENT SOLUTION

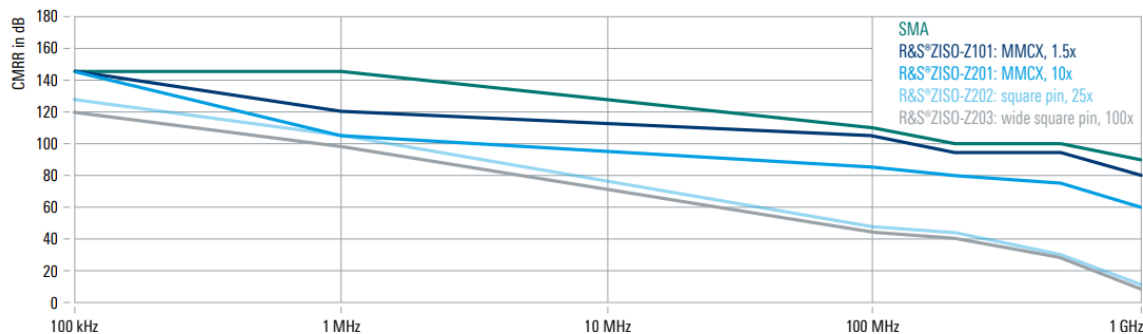
- Fully Optical Isolated Probing System
 - CMMR Of Up to 80dB Is Possible
 - Example:
With 80dB (10000) CMMR @ 40V
Voltage Failure [V] **< 4mV**

- Max. Failure < 0,1% On HS-Gate of GaN Devices

Coax System Is Part Of The Probing Solution



(Source: R&S RT-ZISO Brochure)



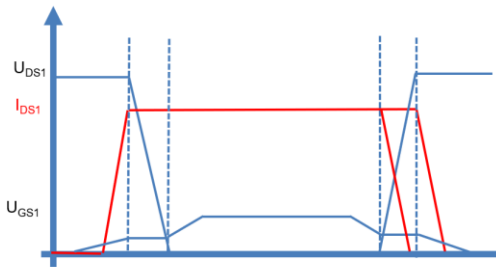
(Source: R&S RT-ZISO Brochure)

THE IMPORTANCE OF SKEW

- ▶ De-Skewing Is Required For Measuring Turn-On and Turn-Off Losses
 - Highly Recommended If Different Probe Types Are Being Used
 - High Impact On Accuracy For Measuring Turn-On and Turn-Off Losses

▶ Current Measurement Solutions:

	Coax Current Shunt	Current Transformer	Rogowski Coil	Infinity
Pros	High Accuracy High Bandwidth	Isolation	• Low Insertion Inductance • Isolation	• Very Low Insertion Inductance
Cons	Large Size Practical Use	Large Size Loop Inductance Low Bandwidth	Low Bandwidth AC Current Only	Design-In Required AC Current Only
Best Use	Switching Losses Evaluation	Lower Bandwidth Applications	Very High Current (DPT) Low Bandwidth	Smaller Application



▶ How To De-Skew For GaN Applications?

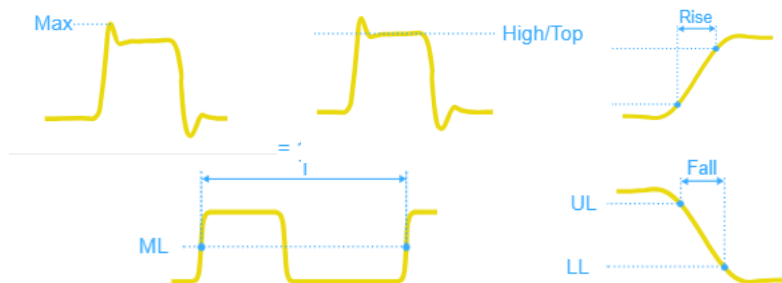
1. Using Data Sheet Values / Values Are Not Accurate Enough To Provide Accurate Skew Figures (E.G < 5ns for A Passive Probe)
2. Using 2 Identical Optical Probes Would Be The Best >> Propagation Delay Is Provided By Probe
3. Perform Multiple Double Pulse Tests And Use Smart Post Processing To Align Voltage & Current (PE-System)

INHERENT MEASUREMENT FUNCTIONS

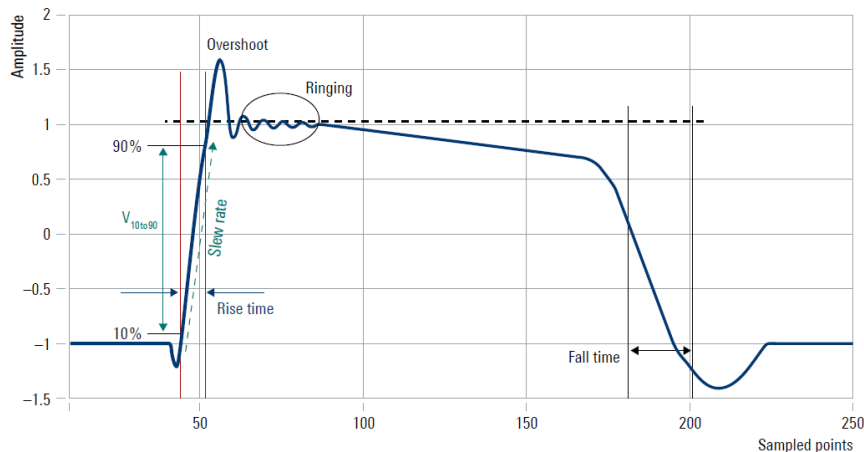
► How To Characterize Devices At Switch Node

- Minimum and Maximum Drain-Source Voltage
- Oscillations
- Rising and Falling Edges (Impact On EMI)

► Automated Measurement Functions Are Useful



(Source: R&S Internal Picture Database)

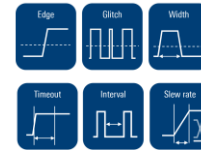
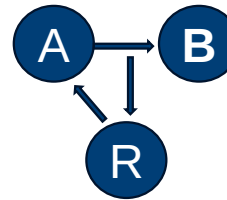
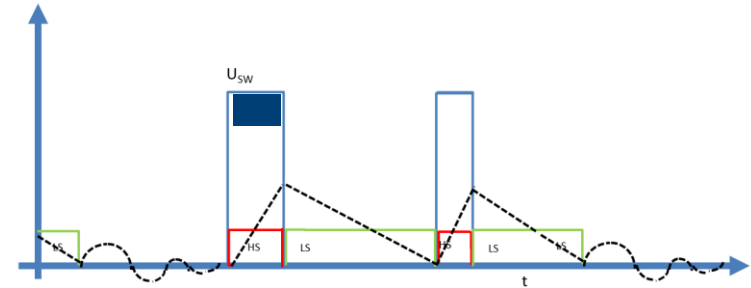


(Source: Marcus Sonst, R&S White Paper "Switching Analysis")

► Fast FFT Implementation

USE OF SMART TRIGGER FUNCTIONS

- ▶ Problem: Converter Changes Operating Mode
 - PWM Frequency and On Time Is Not Stable
 - Simple Edge Trigger Will Fail
- ▶ Solution: Sequence Trigger (A/B-R)
 - Combination of 2 Different Trigger Type
 - In A Sequence With Reset Condition
 - Digital Trigger Implemented In Hardware
- ▶ Alternative >> ZONETRIGGER
 - The Zone trigger triggers on the intersection or non-intersection of the signal and one or more zones

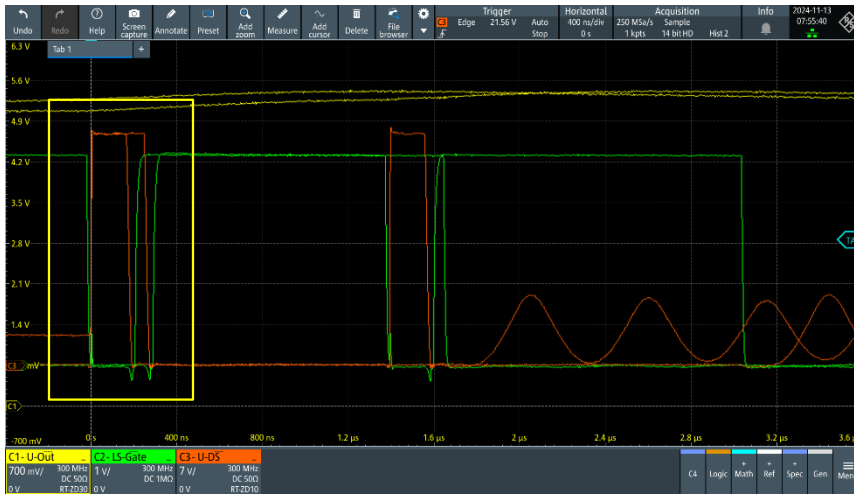


(Source: R&S Internal Picture Database)

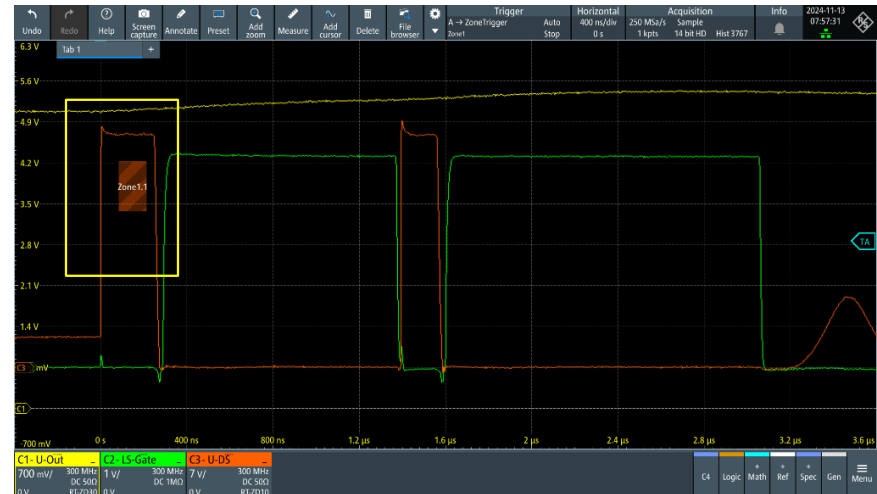
ZONE TRIGGER IN ACTION

- Problem: On-Time Of Duty Cycle Changes Due To Control Loop Of PWM Controller (CCM >> DCM)

Simple Edge Trigger Shows Unclear Result



Trigger With Area Works In Real Time

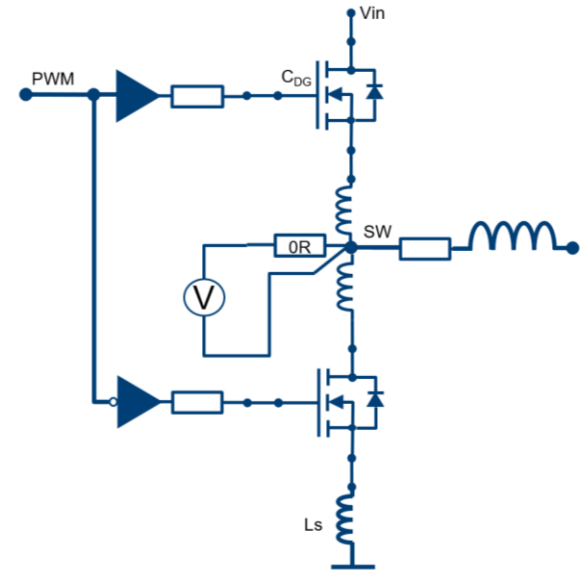


HOW TO PERFORM A CMRR MEASUREMENT

- ▶ How Can Be CMRR Being Measured In A Real Circuit?
 - Validation Of Measurement Equipment Is Performed
A High Voltage Pulse Source (50 Ω System)
(Step Response)
- ▶ In Your Circuit, A Pulse Is Generated By Your Circuit
At The Switch Node
- ▶ All What Needs To Be Done Is To
Connect The Probe (All MMCX Pins)
To The Switch Node

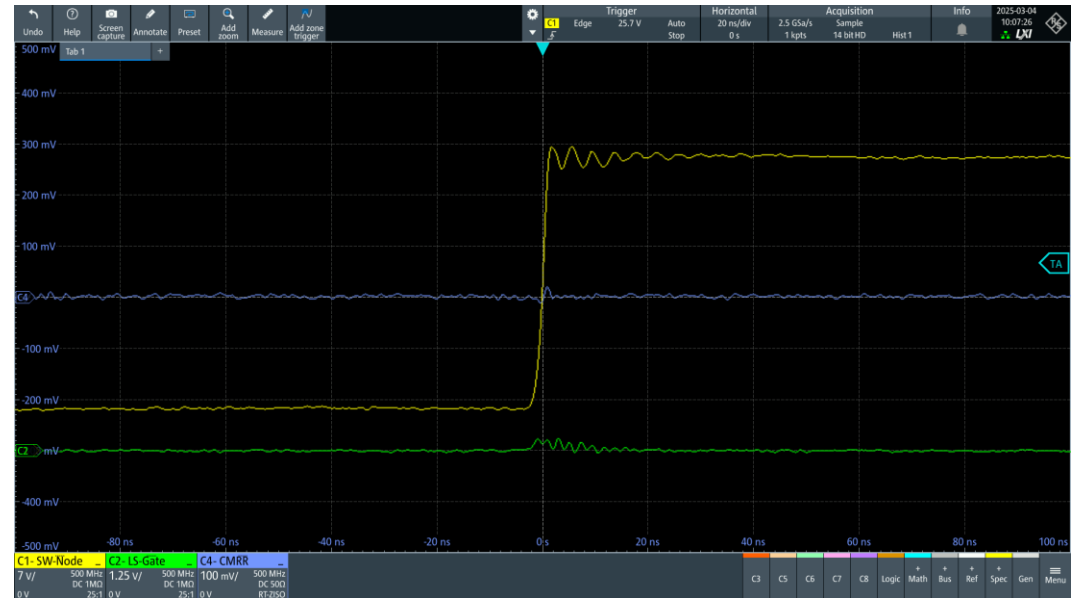
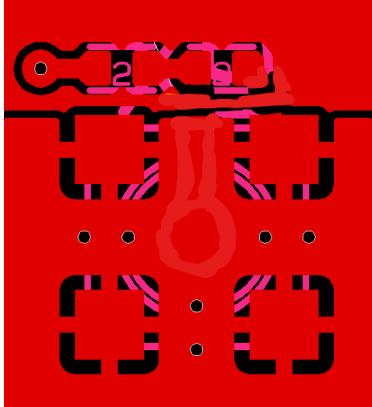
Common-mode rejection ratio

$$CMRR_{dB} = 20 \log_{10} \left(\frac{|A_d|}{|A_{cm}|} \right)$$



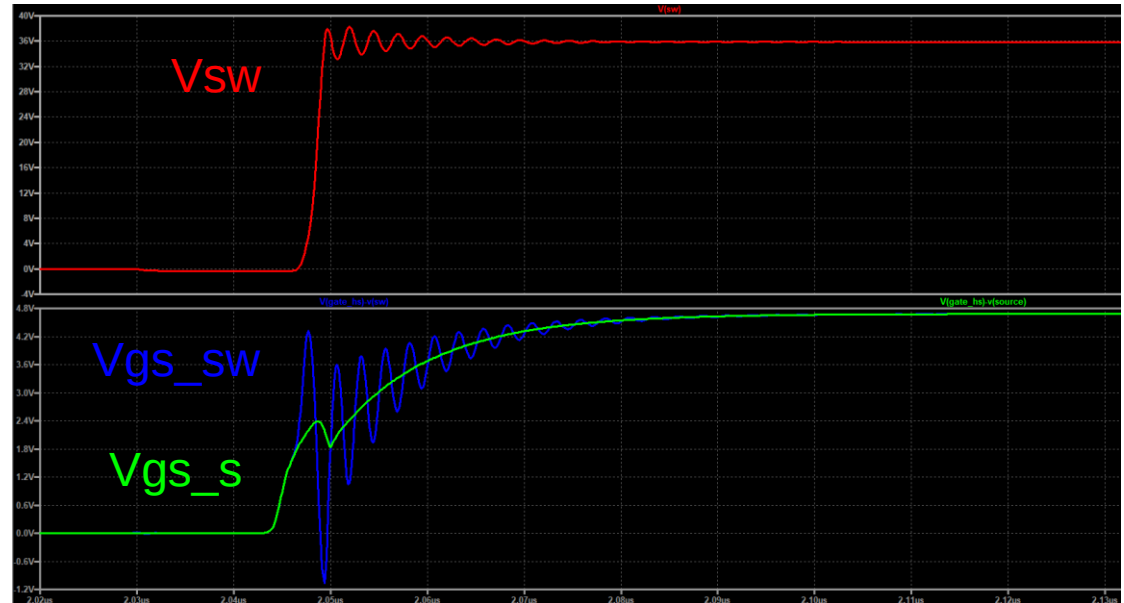
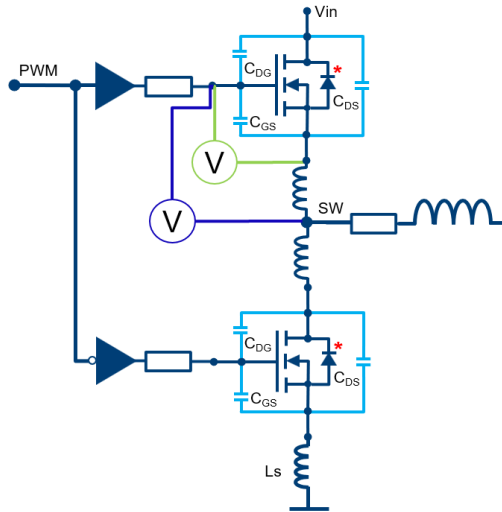
CMRR MEASUREMENT WITH REAL WORLD EXAMPLE)

- ▶ The Configuration Resistor Has Almost 20dB Reduction On CMMR Of The Probe Datasheet
 - It Is Mandatory To Avoid Any Loop
 - Source Impedance Of The Circuit Is Unknown



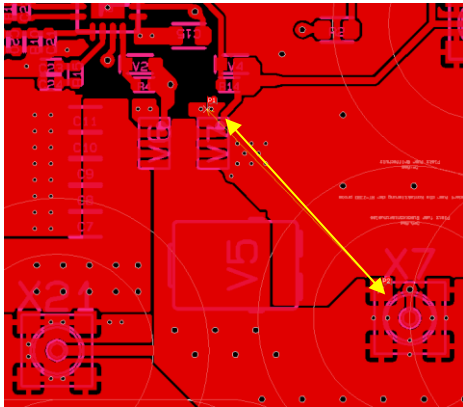
HOW TO CONNECT MMCX TO SWITCH NODE

- Location And Connection Of MMCX Shield Is Critical



HS-GATE RESULT WITH STANDARD PCB LAYOUT

- ▶ MMCX Position Is Not Optimized
 - Track Between Source And MMCX Shield Must Be Of Very Low Impedance
- ▶ 15mm Distance + Vias



PROBE COMPARISON OF HS-GATE MEASUREMENT

High-Side Gate Voltage Measurement With Different Probes with Optimized Probe Location

- ▶ Traditional High Voltage Differential Probe
($f_{BW}=200\text{MHz}$ / $\text{CMRR} = 30\text{dB}$)
- ▶ High Bandwidth / Low Voltage Differential Probe
($f_{BW}=1\text{GHz}$ / $\text{CMRR} = 30\text{dB}$)
- ▶ Fully Isolated Probing System
($f_{BW}=1\text{GHz}$ / $\text{CMRR} = 75\text{dB}$)



CONCLUSION

- ▶ Wide Band Gap Technologies Requires New Measurement Tools And Methods
- ▶ WBG Technology Require Deeper Knowledge Where The Measurement Tools Have Their Limits
- ▶ Probing Technique Has Significant Impact On Signal Fidelity (E.g. Change From Twisted To Coax Cable)
- ▶ It Is Very Challenging To Achieve CMRR Datasheet Values In Real Circuits Because Of Implementation Limits

Find further information:

www.rohde-schwarz.com/oscilloscopes

THANK YOU